

## PATENT ABSTRACTS OF JAPAN

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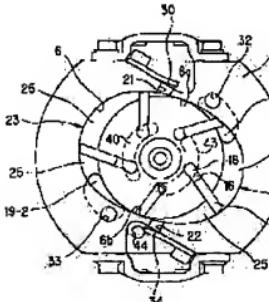
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#### (54) GAS COMPRESSOR

(57) Abstract:

**PROBLEM TO BE SOLVED:** To provide a vane rotary type gas compressor implementing high pressure difference required for a CO<sub>2</sub> refrigeration cycle.

**SOLUTION:** A low pressure intake compressing portion 23 takes therein low pressure CO<sub>2</sub> gas from low pressure intake ports 19, 19-2, compresses the CO<sub>2</sub> gas to be intermediate pressure, and discharges the compressed CO<sub>2</sub> gas to an intermediate pressure discharge port 21. A high pressure compression intake compressing portion 24 takes therein the intermediate pressure CO<sub>2</sub> gas which is discharged from the intermediate pressure discharge port 21, from intermediate pressure intake ports 20, 20-2. The high pressure compression intake compressing portion compresses the intermediate pressure CO<sub>2</sub> to be high pressure, and discharges the high pressure gas to a high pressure discharge port 22. Intermediate pressure CO<sub>2</sub> gas is replenished with CO<sub>2</sub> gas from



an external refrigerant gas supply port 28 to make up for shortage of capacity by two stage compression.

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## DETAILED DESCRIPTION

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### [Detailed Description of the Invention]

[0001]

[Field of the Invention] This invention relates to the suitable gas compressor for refrigerating cycle equipments, such as a car air-conditioner which uses a carbon dioxide (CO<sub>2</sub>) etc. as a refrigerant, an air conditioner, and heat pump.

[0002]

[Description of the Prior Art] In order to prevent contamination of earth environment, division, destruction of an ozone layer, and global warming in recent years, researches and developments of the refrigerating cycle equipment which uses a carbon dioxide with little [ far ] effect (CO<sub>2</sub>) as a refrigerant from chlorofluorocarbon are furthered as a refrigerant used for a car air-conditioner etc.

[0003] As compared with the refrigerating cycle which uses conventional R-22, R-134a, etc. as a refrigerant in the refrigerating cycle which uses a carbon dioxide as a refrigerant, a pressure field is very high, and differential pressure is very large, although low voltage is served as to 3.5-4.0Pa, high pressure serves as 9.0-15MPa and just a compression ratio is small. The piston compressor is the most effective in order to realize big differential pressure efficiently generally, and the researches and developments about the piston compressor for carbon-dioxide refrigerants are prosperous in it.

[0004] Research and development in the refrigerating cycle which used the two-step compressor is also done by making to reduce high pressure on the other hand, without spoiling refrigerating capacity into a key objective.

[0005] The steamy compression equation refrigerating cycle of the two-step compression which used CO<sub>2</sub>, ethylene, ethane, nitrogen oxide, etc. as the refrigerant is indicated by JP,10-288411,A. The outline of this steamy compression equation refrigerating cycle is explained with reference to drawing 8 and drawing 9.

[0006] With a radiator 200, heat is radiated, the high-pressure refrigerant gas (A of drawing 2 ) which the compressor 100 of two-step compression mold compressed the refrigerant gas, and compressed by the 2nd step of compression of this compressor 100 is cooled, and the refrigerant gas (B of drawing 9 ) which passed the radiator 200 is branched to two. A refrigerant is decompressed and injected with a decompression device 300, and a pressure falls, it serves as a vapor-liquid two phase (C of drawing 9 ), and while branching is led to one heat exchange path 400a of a condenser (heat exchanger) 400. The refrigerant of branched another side is led to heat exchange path 400b of another side of a condenser 400.

[0007] When the liquid phase changes to a gaseous phase, endoergic [ of the refrigerant of the vapor-liquid two phase which passes heat exchange path 400a ] is carried out from the refrigerant which passes heat exchange path 400b of another side (D of drawing 9 ), and it is returned to on the way [ of the inhalation pressing operation of a compressor 100 ] (the 2nd step inhalation hole of a compressor 100). The part temperature falls (E of drawing 9 ), and heat exchange path 400b of another side is decompressed with another decompression device (expansion valve) 500 (F of drawing 9 ), carries out endoergic from the outside with the following evaporator (heat sink) 600 (G of drawing 9 ), and returns to the 1st step inhalation hole of a compressor 100 through an accumulator 700.

[0008] A diaphragm of both the decompression devices 400,700 is controlled for branched allocation of a refrigerant and a branched flow rate, and this adjusts the refrigerating capacity of a cycle, and a coefficient of performance to a fitness value.

[0009] In the 2nd step inhalation hole of the above-mentioned compressor 100, the refrigerant ( $H$  of drawing 9) compressed in the 1st step of a compressor 100 and the refrigerant which returns from heat exchange path 400a of a condensator 400 are mixed, and temperature becomes both midpoint ( $J$  of drawing 9). Generally, in the compression stroke of a compressor, temperature also rises with a pressure, the inclination in drawing 9 becomes so large that a compression start point ( $G, J$ ) is in the left of drawing, the point ( $H, A$ ) ending [ part compression ] moves to a left, and its temperature rise decreases. Since compression [ the 2nd step of ] start point of a compressor 100 is  $J$  point with temperature lower than  $H$  points, the work of compression of a compressor 100 is small, a coefficient of performance improves, and the temperature rise of a compressor 100 is also suppressed. The amount of endoergic in an evaporator 600 becomes large with  $F-G$ .

[0010] As a compressor 100 of the above-mentioned two-step compression mold, the scroll type compressor (refer to JP,63-243481,A) which raised a cam-plate mold piston compressor (refer to JP,61-79947,A) and the seal engine performance is adopted.

[0011] The vane rotary mold other than the above-mentioned piston mold and a scroll type is known by the gas compressor. A vane rotary mold gas compressor has the description of simplicity [ structure ], small, and low cost compared with a piston mold. However, it is unsuitable for having to seal a vane rotary mold in the line contact section at the tip of a vane to the piston mold sealing compression space all over the periphery of a piston, and producing big differential pressure.

[0012] When a vane rotary mold gas compressor is used for the refrigerating cycle which uses a carbon dioxide as a refrigerant and measures which the remarkable decline in volumetric efficiency by the gas leakage from compression space and the lack of seal is expected, and lessen leakage as much as possible are taken, power unrelated to compression will increase, or enlargement of a compressor and the increase of weight will be caused, and it becomes impossible to employ the description of vane rotary mold original efficiently.

[0013]

[Problem(s) to be Solved by the Invention] This invention offers conventionally the gas compressor which can realize high differential pressure with ordinary volumetric efficiency, solving an above-mentioned trouble and employing efficiently the easy structure of a vane rotary mold gas compressor, and the original description of being small.

[0014]

[Means for Solving the Problem] In order to solve an above-mentioned technical problem, it sets to the gas compressor of this invention. The cylinder room of a cross-section non-round shape, and Rota which is constructed horizontally across the above-mentioned cylinder interior of a room free [ rotation ] with a rotor shaft, and approaches two or more minor-axis sections of a cylinder indoor peripheral surface with predetermined spacing, Two or more vanes pressed by attitude ease and the cylinder indoor peripheral surface in the vane slot formed in above-mentioned Rota, The discharge opening arranged the inhalation hole arranged near [ one ] the minor-axis section of two or more above-mentioned minor-axis sections, and near [ its / next ] the minor-axis section, It is formed between the cylinder room applied to a discharge opening from the above-mentioned inhalation hole, and Rota. It has two or more inhalation compression zones which pass while the compression space isolation generation is carried out [ compression space ] by Rota rotated in the cylinder interior of a room and the vane changes the volume. In the gas compressor which inhales a refrigerant gas from an inhalation hole, and compression space compresses and carries out the regurgitation

to a discharge opening in an inhalation compression zone The low voltage inhalation compression zone which two or more above-mentioned inhalation compression zones inhale a low-pressure refrigerant gas from a low voltage inhalation hole, compress into the refrigerant gas of intermediate pressure, and carries out the regurgitation to an intermediate pressure discharge opening. It has the high-pressure compression inhalation compression zone which inhales the refrigerant gas supplied from the refrigerant gas and the outside of the above-mentioned intermediate pressure from an intermediate pressure inhalation hole, compresses into a high-pressure refrigerant gas, and carries out the regurgitation to a high-pressure discharge opening. The refrigerant gas supplied is supplied to an intermediate pressure inhalation hole via external refrigerant gas supply opening from the above-mentioned outside.

[0015] It is not necessary to change the volume of the compression space which operates by the low voltage inhalation compression zone, and the compression space which operates by the high-pressure compression inhalation compression zone, and becomes the structure of an easy and small cylinder room as usual, Rota, and a vane by supplying the part whose volume of a refrigerant gas was compressed into intermediate pressure by the low voltage inhalation compression zone, and decreased with a refrigerant gas from the exterior to a high-pressure compression inhalation compression zone. Mutually, the cylinder room of the cross-section ellipse form of a symmetry form, then its configuration are manufactured from the former, and the dimension configuration of the inhalation compression zone of a pair may be the same as what is circulating, and more specifically tends to put a cylinder room in practical use.

[0016] In this gas compressor, moreover, the refrigerant gas of the intermediate pressure breathed out to an intermediate pressure discharge opening The high-pressure refrigerant gas which is supplied to an intermediate pressure inhalation hole once it holds in an intermediate pressure regurgitation room, and is breathed out to a high-pressure discharge opening Once it holds in a high-pressure regurgitation room, it is sent to a delivery. An intermediate pressure oil reservoir room and a high-pressure oil reservoir room are established in the above-mentioned intermediate pressure regurgitation room and a high-pressure regurgitation room, respectively. If it is made for a back pressure room for the lubricating oil of the above-mentioned intermediate pressure oil reservoir room to press a vane while passing a low voltage inhalation compression zone to be supplied at a back pressure room for the lubricating oil of a high-pressure oil reservoir room to press a vane while passing a high-pressure compression inhalation compression zone The thrust to a cylinder room becomes strong moderately according to a compression pressure about a vane, and seal with compression space and the next compression space is improved by comparatively little power loss.

[0017] in addition, in this invention, it has "two or more minor-axis sections" -- "-- the inhalation compression zone for those intermediate pressure is prepared between a low voltage inhalation compression zone and a high-pressure compression inhalation compression zone, or the refrigerant gas of the intermediate pressure from two low voltage inhalation compression zones and these two low voltage inhalation compression zones is doubled, and it is made to send to the cylinder room of cross-section un-circular" in this case to a high-pressure compression inhalation compression zone including the cylinder room of for example, the conclusion form

[0018] Although the gas compressor of this invention is applicable also to the refrigerating cycle which carries out heat exchange of the refrigerant gas returned to the 2nd step of above-mentioned compression through a condensator 400, it does not necessarily need to let a condensator pass.

[0019]

[Embodiment of the Invention] The gestalt of implementation of this invention is hereafter explained with reference to drawing 1 - drawing 7.

[0020] The II-II line sectional view of drawing 1 and drawing 3 of drawing of longitudinal section in which drawing 1 shows the gestalt of 1 implementation of this invention, and drawing 2 are block diagrams in which the III-III line sectional view, drawing 4, drawing 5, and drawing 6 of drawing 1 show A \*\*\*\* Fig. of the rear side block of the gas compressor of drawing 1, a frontside block, and a front head, and drawing 7 shows the two-step compression stroke of the gas compressor of drawing 1, respectively.

[0021] For a cylinder block 1 as for a frontside block and 4, in drawing 1, a rear side block and 3 are [ 1 ] a front head and 5 ] casing.

[0022] As a cylinder block 1 is closed by the rear side block 2 and the frontside block 3 and shows a both-ends side to drawing 2, the cylinder room 6 of a cross-section ellipse form is mostly formed in the interior. The outside end face of the above-mentioned rear side block 2 is closed by the above-mentioned casing 5, and the high-pressure regurgitation room 7 is formed between the rear side block 2 and casing 5. Moreover, the outside end face of the frontside block 3 is closed by the above-mentioned front head 4, and the intermediate pressure regurgitation room 8 is formed between the frontside block 3 and the front head 4.

[0023] 9 is Rota, and this Rota 9 is constructed across horizontally free [ rotation ] in the above-mentioned cylinder room 6 with a rotor shaft 10, and is close to two or more minor-axis sections explained after the inner skin of the cylinder room 6 with predetermined spacing. The above-mentioned rotor shaft 10 is supported by the bearing 11 of the rear side block 2, and the bearing 12 of the frontside block 3, and a front-side is extended to the front head 4 side, it engages with the electromagnetic clutch 13 with which the front head 4 was equipped, the rotational motion force of the engine of an automobile is transmitted through a belt 14, a pulley 15, and an electromagnetic clutch 13, and it rotates Rota 9 in the cylinder room 6.

[0024] The detail of the [cylinder indoor section], next the cylinder room 6 interior is explained.

[0025] As shown in drawing 2, five vane slots 16 are formed in Rota 9 at the radial leaned a little from the Rota core. Attitude ease and the vane 17 which \*\*\*\*s to the inner skin of the cylinder room 6 are inserted in these vane slots 16 in Mizouchi. Moreover, the two minor-axis sections 6a and 6b of the inner skin of the cross-section \*\*\*\* elliptical cylinder room 6 serve as a circular face of the Rota shaft center, and the outer-diameter section of Rota 9 is close with these minor-axis sections 6a and 6b and predetermined spacing.

[0026] The back pressure room 18 is established in the pars basilaris ossis occipitalis of the above-mentioned vane slot 16, and according to the angular position in the cylinder room 6, suitable back pressure is added to this back pressure room 18 at so that it may explain to a detail later.

[0027] The inhalation holes 19 and 20, 19-2, and 20-2 are arranged near the above-mentioned minor-axis sections 6a and 6b and in the travelling direction in Rota 9 by both side blocks 2 and 3 ( drawing 4 , R> drawing 5 5 reference). Moreover, discharge openings 21 and 22 are arranged in the opposite side of near the minor-axis sections 6a and 6b, the inhalation holes 19 and 20, 19-2, and 20-2 by the cylinder block 1, and from the inhalation hole 19 near [ one ] minor-axis section 6a (or 6b), and 19-2 (20 or 20-2) Between the cylinder room 6 applied to the discharge opening 22 (or 21) arranged near [ the / next ] minor-axis section 6b (or 6a), and Rota 9 Two or more inhalation compression zones 23 and 24 are formed, and while the compression space 25 isolation generation is carried out [ the compression space ] by Rota 9 rotated in the cylinder room 6 and 1 set of vanes 17 and 17 changes the volume to these inhalation compression zones 23 and 24, it passes.

[0028] The passage of the refrigerant of this gas compression inside of a plane is explained referring to [the two-step compression process of the passage of a refrigerant, and a refrigerant], next drawing 7.

[0029] Drawing 1, the inhalation opening 26 shown in drawing 3, the delivery 27 shown in drawing 1, and the external refrigerant gas supply opening 28 are carrying out opening to the gas compressor, and it connects with piping of a refrigeration system. For example, when using it for the refrigeration system shown in drawing 8, the external refrigerant gas supply opening 28 is connected to piping which leads to heat exchange path 400a of a condenser 400 again at piping which leads a delivery 27 to a radiator 200 at piping which leads the inhalation opening 26 to an accumulator 700, respectively.

[0030] The inhalation opening 26 connected to the low-tension side of a refrigeration system is open for free passage to the above-mentioned inhalation hole 19 through the inhalation opening free passage way 29 and the free passage hole 31 of the frontside block 3, this inhalation hole 19 is the low voltage inhalation hole which inhales a low voltage refrigerant gas, and the inhalation compression zone 23 with the low voltage inhalation hole 19 has become in it with the low voltage inhalation compression zone which inhales and compresses a low voltage refrigerant gas. In addition, the low voltage inhalation hole 19-2 by the side of the rear side block 2 is also open for free passage with the cylinder block low voltage free passage way 33 penetrated to the cylinder block 1 with the low voltage inhalation hole 19 by the side of the frontside block 3. The delivery 27 connected to the high-tension side of a refrigeration system is open for free passage in the above-mentioned high-pressure regurgitation room 7. The external refrigerant gas supply opening 28 connected to the intermediate pressure side of a refrigeration system is open for free passage in the above-mentioned intermediate pressure regurgitation room 8.

[0031] The discharge opening 21 of the low voltage inhalation compression zone 23 is the intermediate pressure discharge opening which carries out the regurgitation of the refrigerant gas compressed into intermediate pressure, and is open for free passage in the above-mentioned intermediate pressure regurgitation room 8 through a discharge valve 30 and the free passage way 47. In addition, the above-mentioned discharge valve 30 is a well-known discharge valve conventionally which consists of a little thick valve guide which stops and backs up the valve seat formed on the outskirts of discharge opening 21 of a cylinder block 1, a lead valve, and the excessive knee of this lead valve.

[0032] The inhalation hole 20 of another inhalation compression zone 24 is also open for free passage in the intermediate pressure regurgitation room 8, and the intermediate pressure inhalation hole with which this inhalation hole 20 inhales middle pressure refrigerant gas, and the inhalation compression zone 24 are the high-pressure compression inhalation compression zone which compresses a refrigerant gas into high pressure from intermediate pressure.

[0033] In addition, the above-mentioned inhalation hole 19 of the frontside block 2, the above-mentioned inhalation hole 19-2 of the rear side block 2, and the intermediate pressure inhalation hole 20-2 serve as a hollow established in the end face which faces the cylinder room 6 of both side blocks 2 and 3, respectively, and it penetrates and they are opening the above-mentioned inhalation hole 20 of the frontside block 2 for free passage with the intermediate pressure regurgitation room 8.

[0034] The intermediate pressure inhalation hole 20 by the side of the rear side block 2 is open for free passage with the cylinder block intermediate pressure free passage way 32 penetrated to the cylinder block 1 with the intermediate pressure inhalation hole 20 by the side of the frontside block 3.

[0035] The high-pressure discharge opening 22 of the high-pressure compression inhalation

compression zone 24 is open for free passage with the high-pressure regurgitation room 7 through a discharge valve 34 (refer to drawing 2 ), the high-pressure refrigerant paths 44, 45, and 46 (refer to drawing 4 ), and an oil separator 35 (refer to drawing 1 ). In addition, the above-mentioned discharge valve 34 is a well-known discharge valve conventionally which consists of a little thick valve guide which stops and backs up the valve seat formed on the outskirts of discharge opening 22 of a cylinder block 1 like the discharge valve 30, a lead valve, and the excessive knee of this lead valve.

[0036] Refrigerant inhalation / compression actuation of a gas compressor is as follows.

[0037] By rotation of Rota 9 of a gas compressor, the compression space 25 located in the low voltage inhalation compression zone 23 is followed on rotation of Rota 9, and they are the low voltage inhalation hole 19 and CO2 of 19-2 to about 3.5 MPa(s) at a volume increasing process. A refrigerant gas is inhaled, this is compressed into intermediate pressure in a volume decrease process, and it sends into the intermediate pressure regurgitation room 8 through a discharge valve 30 from the intermediate pressure discharge opening 21. The refrigerant of intermediate pressure is sent into this intermediate pressure regurgitation room 8 from the external refrigerant feed hopper 28, and when compressing into 10MPa(s) from 3.5MPa, it is controlled by the decompression device of a refrigeration system so that intermediate pressure is mostly set to that middle 6.5-7MPa.

[0038] In the meantime, in the compression space 25 located in the high-pressure compression inhalation compression zone 24, the refrigerant gas of about 6.5 MPa(s) of the intermediate pressure regurgitation room 8 is inhaled from the intermediate pressure inhalation hole 20 and 20-2 by the volume increasing process, this is compressed into the high pressure of about 10 MPa(s) in a volume decrease process, and it sends into the high-pressure regurgitation room 7 through a discharge valve 34 and an oil separator 35 from the high-pressure discharge opening 22. The high-pressure refrigerant of about 10 MPa(s) of the high-pressure regurgitation room 7 is sent out from a delivery 27 outside.

[0039] Thus, compression of high differential pressure, such as 3.5MPa to 10MPa(s), is realizable with two steps of compression, the 1st-step compression of the low voltage inhalation compression zone 23 and compression of the 2nd step of the high-pressure compression inhalation compression zone 24. An intermediate pressure is automatically adjusted by the flow rate of the refrigerant gas which flows from the external refrigerant gas supply opening 28, and the volume of the compression space of the 1st step and the 2nd step can be made the same.

[0040] A vane 17 is pressed by the cylinder indoor peripheral surface in the [back pressure and lubrication] above-mentioned gas compressor. In addition to the centrifugal force by rotation of the vane itself, this thrust is based on the back pressure which joins the back pressure room 18. As for this back pressure, in the low voltage inhalation compression zone 23, considering as mist or low voltage is more desirable than the high-pressure compression inhalation compression zone 24. Because, although the seal of a vane and a cylinder room will become good in the low voltage inhalation compression zone 23 if not much high back pressure is applied to the pressure to compress overcoming a pressure of this level, and pressing a vane 17 to a cylinder indoor peripheral surface like 6.5MPa(s) It is because back pressure higher [ the pressure compressed by the high-pressure compression inhalation compression zone 24 to power loss becoming large too much is as high as / like 10MPa(s) /, and ] in order to overcome this high pressure and to press a vane 17 to a cylinder indoor peripheral surface is required.

[0041] So, in this invention, the high-pressure oil reservoir room 37 is established in the pars basilaris ossis occipitalis of the intermediate pressure regurgitation room 8 at the pars basilaris ossis occipitalis of the intermediate pressure oil reservoir room 36 and the high-

pressure regurgitation room 7. The back pressure room 18 for the lubricating oil of the high-pressure oil reservoir room 37 to press the vane 17 while passing the high-pressure compression inhalation compression zone 24 is supplied at the back pressure room 18 for the lubricating oil of the intermediate pressure oil reservoir room 36 to press the vane 17 while passing the low voltage inhalation compression zone 23.

[0042] That is, the lubricating oil of the intermediate pressure oil reservoir room 36 carries out the lubrication of the bearing, it is further decompressed with the front diaphragm hole 39, is sent [ it is sent to bearing 12 from the front oil gallery 38, and ] to the middle back pressure oil supply crevice 40 of both side blocks 2 and 3, and is supplied to the back pressure room 18 under low voltage inhalation compression zone 23 passage which touches this middle back pressure oil supply crevice 40. On the other hand, the lubricating oil of the high-pressure oil reservoir room 37 carries out the lubrication of the bearing, it is further decompressed with the rear diaphragm hole 42, is sent [ it is sent to bearing 11 from the rear oil gallery 41, and ] to the high back pressure oil supply crevice 43 of both side blocks 2 and 3, and is supplied to the back pressure room 18 under high-pressure compression inhalation compression zone 24 passage which touches this middle back pressure oil supply crevice 43. In addition, the supply way of the middle back pressure oil to the middle back pressure oil supply crevice 40 of the rear side block 2 and the supply way of the high back pressure oil to the high back pressure oil supply crevice 43 of the frontside block 3 omit illustration.

[0043] The pressure of the middle back pressure oil supply crevice 40 is lower than the pressure of the high back pressure oil supply crevice 43, the back pressure to which the vane while passing the low voltage inhalation compression zone 23, and the vane while passing the high-pressure compression inhalation compression zone 24 suited each is applied, and the seal of a good vane and a cylinder room is secured without excessive power loss.

[0044] In addition, the lubricating oil which begins to leak from the back pressure room 17 is used also for the lubrication of the sliding surface of Rota 9 and a vane 17, and the sliding surface of a vane 17 and the cylinder room 6. Moreover, the lubricating oil of the intermediate pressure oil reservoir room 36 and the high-pressure oil reservoir room 37 is sent also to Rota 9 and the slide contact side of a vane 17 and both side blocks 2 and 3 through the path of an illustration abbreviation, and is used also for the lubrication. It is separated from a refrigerant by the above-mentioned oil separator 35, and a lubricating oil is returned to the high-pressure oil reservoir room 37. Recovery of the lubricating oil to the intermediate pressure oil reservoir room 36 is based on separation recovery from the refrigerant once held in the intermediate pressure regurgitation room 8.

[0045] [Effect of the Invention] As explained to the detail above, the gas compressor of this invention While two or more compression space of the equal volume carries out sequential passage of a low voltage inhalation compression zone and the high-pressure compression inhalation compression zone mutually, in a low voltage inhalation compression zone A low-pressure refrigerant gas is inhaled from a low voltage inhalation hole, and it compresses into the refrigerant gas of intermediate pressure. To an intermediate pressure discharge opening in discharge and a high-pressure compression inhalation compression zone Since the refrigerant gas for a supplement supplied from the above-mentioned refrigerant gas and the above-mentioned outside of intermediate pressure is inhaled from an intermediate pressure inhalation hole, it compresses into a high-pressure refrigerant gas and it was made to carry out the regurgitation to a high-pressure discharge opening The same Rota as the vane rotary mold gas compressor using the conventional refrigerants, such as chlorofluocarbon, the vane, and the cylinder could be used, and it could be easy, and could consider as low cost and a small gas compressor, and the gas compressor of the high differential pressure which used a

carbon dioxide, ethylene, ethane, nitrogen oxide, etc. as the refrigerant has been realized.

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## CLAIMS

[Claim(s)]

[Claim 1] The cylinder room of a cross-section non-round shape, and Rota which is constructed horizontally across the above-mentioned cylinder interior of a room free [ rotation ] with a rotor shaft, and approaches two or more minor-axis sections of a cylinder indoor peripheral surface with predetermined spacing. Two or more vanes pressed by attitude ease and the cylinder indoor peripheral surface in the vane slot formed in above-mentioned Rota, The discharge opening arranged the inhalation hole arranged near [ one ] the minor-axis section of two or more above-mentioned minor-axis sections, and near [ its / next ] the minor-axis section. It is formed between the cylinder room applied to a discharge opening from the above-mentioned inhalation hole, and Rota. It has two or more inhalation compression zones which pass while the compression space isolation generation is carried out [ compression space ] by Rota rotated in the cylinder interior of a room and the vane changes the volume. In the gas compressor which inhales a refrigerant gas from an inhalation hole, and compression space compresses and carries out the regurgitation to a discharge opening in an inhalation compression zone The low voltage inhalation compression zone which two or more above-mentioned inhalation compression zones inhale a low-pressure refrigerant gas from a low voltage inhalation hole, compress into the refrigerant gas of intermediate pressure, and carries out the regurgitation to an intermediate pressure discharge opening. It has the high-pressure compression inhalation compression zone which inhales the refrigerant gas supplied from the refrigerant gas and the outside of the above-mentioned intermediate pressure from an intermediate pressure inhalation hole, compresses into a high-pressure refrigerant gas, and carries out the regurgitation to a high-pressure discharge opening. It is the gas compressor characterized by supplying the refrigerant gas supplied to an intermediate pressure inhalation hole via external refrigerant gas supply opening from the above-mentioned outside.

[Claim 2] The refrigerant gas of the intermediate pressure breathed out to an intermediate pressure discharge opening The high-pressure refrigerant gas which is supplied to an intermediate pressure inhalation hole once it holds in an intermediate pressure regurgitation room, and is breathed out to a high-pressure discharge opening Once it holds in a high-pressure regurgitation room, it is sent to a delivery. An intermediate pressure oil reservoir room and a high-pressure oil reservoir room are established in the above-mentioned intermediate pressure regurgitation room and a high-pressure regurgitation room, respectively. The gas compressor according to claim 1 characterized by supplying a back pressure room for the lubricating oil of the above-mentioned intermediate pressure oil reservoir room

pressing a vane while passing a low voltage inhalation compression zone at a back pressure room for the lubricating oil of a high-pressure oil reservoir room pressing a vane while passing a high-pressure compression inhalation compression zone.

[Claim 3] The gas compressor according to claim 1 whose cross-section non-round shape is an ellipse form.

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#### DESCRIPTION OF DRAWINGS

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[Brief Description of the Drawings]

[Drawing 1] Drawing of longitudinal section showing the gestalt of 1 implementation of this invention.

[Drawing 2] The II-II line sectional view of drawing 1.

[Drawing 3] The III-III line sectional view of drawing 1.

[Drawing 4] A \*\*\*\* Fig. of a rear side block of drawing 1.

[Drawing 5] A \*\*\*\* Fig. of a frontside block of drawing 1.

[Drawing 6] A \*\*\*\* Fig. of the front head of drawing 1.

[Drawing 7] The explanatory view of the steamy compression equation refrigerating cycle of the method which returns a refrigerant to a two-step pressing operation.

[Drawing 8] The block diagram showing the two-step compression stroke of the gas compressor of drawing 1.

[Drawing 9] The Mollier chart of the steamy compression equation refrigerating cycle of drawing 6.

[Description of Notations]

6 Cylinder Room

6a Minor-axis section

6b Minor-axis section

7 High-Pressure Regurgitation Room

8 Intermediate Pressure Regurgitation Room

9 Rota

10 Rotor Shaft

16 Vane Slot

17 Vane

18 Back Pressure Room

19 Low Voltage Inhalation Hole

19-2 Low Voltage Inhalation Hole

20 Intermediate Pressure Inhalation Hole

20-2 Intermediate Pressure Inhalation Hole

- 21 Intermediate Pressure Discharge Opening
- 22 High-Pressure Discharge Opening
- 23 Low Voltage Inhalation Compression Zone
- 24 High-Pressure Compression Inhalation Compression Zone
- 25 Compression Space
- 26 Inhalation Opening
- 27 Delivery
- 28 External Refrigerant Gas Supply Opening
- 36 Intermediate Pressure Oil Reservoir Room
- 37 High-Pressure Oil Reservoir Room
- 100 Compressor
- 200 Radiator
- 400 Condensator
- 600 Evaporator

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[Translation done.]

(19)日本国特許庁 (JP)

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	3 6 1		3 6 1 G
F 2 5 B 1/00	3 9 5	F 2 5 B 1/00	3 9 5 Z
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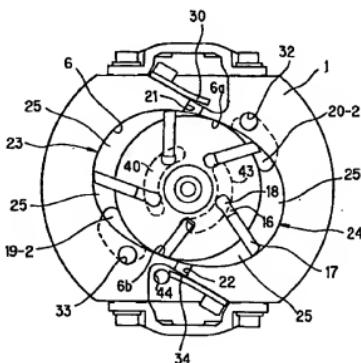
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## (54)【説明の名稱】 気体圧縮機

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## (57)【要約】

【課題】 CO<sub>2</sub> 冷凍サイクルに必要な高い圧力差を実現できるペーンロータリ型気体圧縮機を提供する。【解決手段】 低圧吸入口部23は、低圧吸入口19、19-2から低圧CO<sub>2</sub>ガスを吸入して中間圧に圧縮し、中間圧吐出孔21に吐出する。高圧圧縮吸入圧縮部24は、中間圧吐出孔21から吐出した中間圧CO<sub>2</sub>ガスを中間圧吸入口20、20-2から吸入して高圧に圧縮し、高圧吐出孔22に吐出する。中間圧CO<sub>2</sub>ガスには外部冷媒ガス供給口28からCO<sub>2</sub>ガスを補充し、2段圧縮による容量不足を補う。

## 【特許請求の範囲】

【請求項1】 断面非円形のシリング室と、上記シリング室内にロータ軸により回転自在に構成され、シリング室内周面の複数の短径部に所定の間隔をもって近接するロータと、上記ロータに形成されたベーン溝に進退自在、かつ、シリング室内周面に押される複数のベーンと、上記複数の短径部のうちのひとつ短径部付近に配設された吸込孔およびその隣の短径部付近に配設された吐出孔と、上記吸込孔から吐出孔にかけてのシリング室とロータとの間に形成され、シリング室内で回転するロータとベーンにより隔壁生成される圧縮室がその体積を変化させながら通過する複数の吸入圧縮部とを有し、吸入圧縮部において圧縮室が吸込孔から冷媒ガスを吸入し、圧縮して吐出孔に吐出する気体圧縮機において、上記複数の吸入圧縮部が、

低圧の冷媒ガスを低圧吸込孔から吸入して中間圧の冷媒ガスに圧縮して中間圧吐出孔へ吐出する低圧吸入圧縮部と、

上記中間圧の冷媒ガスおよび外部から供給される冷媒ガスを中間圧吸込孔から吸入して高圧の冷媒ガスに圧縮して高圧吐出孔へ吐出する高圧圧縮吸入圧縮部とを有し、上記外部から供給される冷媒ガスは、外部冷媒ガス供給口を経由して中間圧吸込孔へ供給されるようになっていことを特徴とする気体圧縮機。

【請求項2】 中間圧吐出孔へ吐出される中間圧の冷媒ガスは、中間圧吐出室に一旦収容されてから中間圧吸込孔へ供給され、

高圧吐出孔へ吐出される高圧の冷媒ガスは、高圧吐出室に一旦収容されてから吐出口へ送られるようになっており、

上記中間圧吐出室および高圧吐出室にはそれぞれ中間圧油貯留室および高圧油貯留室が設けられ、

上記中間圧油貯留室の潤滑油が低圧吸入圧縮部を通過中のベーンを押圧するための背压室へ、高圧油貯留室の潤滑油が高圧圧縮吸入圧縮部を通過中のベーンを押圧するための背压室へ供給されるようになっていることを特徴とする請求項1記載の気体圧縮機。

【請求項3】 断面非円形が楕円形である請求項1記載の気体圧縮機。

## 【発明の詳細な説明】

## 【0001】

【発明の属する技術分野】 この発明は、二酸化炭素 ( $\text{CO}_2$ ) 等を冷媒として使用するカーエアコン、空調装置、ヒートポンプ等の冷凍サイクル装置に好適な気体圧縮機に関する。

## 【0002】

【從来の技術】 近年、地球環境の汚染、とりわけ、オゾン層の破壊、地球温暖化を防止するために、カーエアコン等に使用する冷媒として、フロンによる影響の少ない二酸化炭素 ( $\text{CO}_2$ ) を冷媒とする冷凍サイクル

装置の研究開発が進められている。

【0003】 二酸化炭素を冷媒とする冷凍サイクルでは、従来の R-22 や R-134a 等を冷媒とする冷凍サイクルと比較して圧力領域が非常に高く、低圧は 3.5 ~ 4.0 MPa、高圧は 9.0 ~ 15 MPa となり、圧縮比こそ小さいものの圧力差が非常に大きい。ビストン圧縮機は、一般に大きな圧力差を効率よく実現するため最も有利であり、二酸化炭素冷媒用のビストン圧縮機に関する研究開発が盛んである。

【0004】 一方、冷凍能力を損なわずに高圧を低下させることが主目的として、2段圧縮機を使用した冷凍サイクルも研究開発されている。

【0005】 特開平10-288411号公報には、 $\text{CO}_2$ 、エチレン、エタン、酸化窒素等を冷媒とした2段圧縮の蒸気圧縮式冷凍サイクルが開示されている。この蒸気圧縮式冷凍サイクルの概要を図8および図9を参照して説明する。

【0006】 2段圧縮型の圧縮機 100 が冷媒ガスを圧縮し、この圧縮機 100 の2段目の圧縮により圧縮した

20 高圧冷媒ガス(図9のA)を放熱器 200 で放熱して冷却し、放熱器 200 を通過した冷媒ガス(図9のB)をふたつに分岐する。分岐した一方の冷媒は、減圧装置 30.0 で減圧して噴射され、圧力が下がって液相二相となり(図9のC)、冷却器(熱交換器)400の一方の熱交換通路 400a へ導かれる。分岐した他方の冷媒は、冷却器 400 の他方の熱交換通路 400b へ導かれる。

【0007】 熱交換通路 400a を通過する気液二相の冷媒は、液相が気相に変化することにより、他方の熱交換通路 400b を通過する冷媒から吸熱し(図9のD)、

30 圧縮機 100 の吸入圧縮工程の途中(圧縮機 100 の2段目吸込孔)に戻される。他方の熱交換通路 400b はその分温度が下がって(図9のE)、別の減圧装置(膨胀弁)500で減圧し(図9のF)、次の蒸発器(吸熱器)600で外部から吸熱して(図9のG)、アクチュレータ 700 を介して圧縮機 100 の1段目吸込孔に戻る。

【0008】 分岐される冷媒の分配や流量を、両減圧装置 400、700 の絞りを制御し、これによりサイクルの冷凍能力、成績係数を適性値に調節する。

40 【0009】 上記の圧縮機 100 の2段目吸込孔では、圧縮機 100 の1段目で圧縮された冷媒(図9のH)と冷却器 400 の熱交換通路 400a から戻ってくる冷媒とが混合され、温度が両者の中間点(図9のJ)になる。一般に圧縮機の圧縮行程では、圧力とともに温度も上昇し、図9におけるその勾配は、圧縮開始点(G、J)が左方にある程大きくなり、その分圧縮終了点(H、A)は左方へ移動して、温度上昇が少なくなる。圧縮機 100 の2段目の圧縮開始点は、H 点より温度の低い J 点であるから、圧縮機 100 の圧縮仕事は小さく、成績係数が向上し、圧縮機 100 の温度上昇も抑え

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られる。蒸発器600での吸熱量はF-Gと大きくなる。

【0010】上記の2段圧縮型の圧縮機1000としては、斜板型ピストン圧縮機（特開昭61-79947号公報参照）やシール性能を向上させたスクロール型圧縮機（特開昭63-243481号公報参照）が採用されている。

【0011】気体圧縮機には、上記のピストン型、スクロール型の他に、ペーンロータリ型が知られている。ペーンロータリ型気体圧縮機は、ピストン型に比べて構造が簡単、小型、低コストという特徴を有する。しかし、ピストン型がピストンの外周面で圧縮室の密封を行っているのに対し、ペーンロータリ型は、ペーン先端の線接触部で密封しなければならず、大きな圧力差を生じさせるには不向きである。

【0012】二酸化炭素を冷媒とする冷冻サイクルにペーンロータリ型気体圧縮機を用いた場合、圧縮室からのガス漏れ、密封不足による著しい体積効率の低下が予想され、また、漏れを極力少なくするような対策をとると、圧縮とは無関係な動力が増えたり、圧縮機の大形化、重量増を招くことになり、ペーンロータリ型本来の特徴を生かすことができなくなる。

### 【0013】

【発明が解決しようとする課題】この発明は、上述の問題点を解決し、ペーンロータリ型気体圧縮機の簡単な構造、小型という本来の特徴を生かしながら、従来並みの体積効率で高い圧力差を実現できる気体圧縮機を提供するものである。

### 【0014】

【課題を解決するための手段】上述の課題を解決するために、この発明の気体圧縮機においては、断面非円形のシリンドラ室と、上記シリンドラ室内にロータ軸により回転自在に横架され、シリンドラ室内周面の複数の短径部に所定の間隔をもって近接するロータと、上記ロータに形成されたペーン溝に進退自在、かつ、シリンドラ室内周面上に押圧される複数のペーンと、上記複数の短径部のうちのひとつの短径部付近に配設された吸入孔およびその隣の短径部付近に配設された吐出孔と、上記吸入孔から吐出孔にかけてのシリンドラ室とロータとの間に形成され、シリンドラ室内で回転するロータとペーンにより隔壁生成される圧縮室がその体積を変化させながら通過する複数の吸入圧縮部とを有し、吸入圧縮部において圧縮室が吸入孔から冷媒ガスを吸入り、圧縮して吐出孔に吐出する気体圧縮機において、上記複数の吸入圧縮部が、低圧の冷媒ガスを低圧吸入孔から吸入して中間圧の冷媒ガスに圧縮して中間圧吐出孔へ吐出する低圧吸入圧縮部と、上記中間圧の冷媒ガスおよび外部から供給される冷媒ガスを中間圧吸入孔から吸入して高圧の冷媒ガスに圧縮して高圧吐出孔へ吐出する高圧圧縮吸入圧縮部とを有し、上記外部から供給される冷媒ガスは、外部冷媒ガス供給口を

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経由して中間圧吸入孔へ供給されるようになっている。

【0015】低圧吸入圧縮部で中間圧に圧縮され冷媒ガスの体積が減った分を、高圧圧縮吸入圧縮部へ外部から冷媒ガスで補充することにより、低圧吸入圧縮部で作動する圧縮室と高圧圧縮吸入圧縮部で作動する圧縮室との体積を変える必要がなく、従来どおりの簡単なシリンドラ室、ロータ、ペーンの構造となる。より具体的には、例えば、シリンドラ室を一対の吸入圧縮部の寸法形状が互いに対称形の断面非円形のシリンドラ室とすれば、その形状が従来から製造され、流通しているものと同じでよいことになり、実用化しやすいものになる。

【0016】また、この気体圧縮機において、中間圧吐出孔へ吐出される中間圧の冷媒ガスは、中間圧吐出室に一旦収容されてから中間圧吸入孔へ供給され、高圧吐出孔へ吐出される高圧の冷媒ガスは、高圧吐出室に一旦収容されてから吐出孔へ送られるようになっており、上記中間圧吐出室および高圧吐出室にはそれぞれ中間圧油貯留室および高圧油貯留室が設けられ、上記中間圧油貯留室の潤滑油が低圧吸入圧縮部を通過中のペーンを押圧するための背压室へ、高圧油貯留室の潤滑油が高圧圧縮吸入圧縮部を通過中のペーンを押圧するための背压室へ供給されるようになると、ペーンをシリンドラ室への押圧力が圧縮圧力に応じて適度に強まり、比較的少ない動力損で圧縮室と隣の圧縮室との密封が改善される。

【0017】なお、この発明において、「複数の短径部」を有する「断面非円形」のシリンドラ室には、例えば、おむすび形のシリンドラ室を含み、この場合は、低圧吸入圧縮部と高圧圧縮吸入圧縮部との間に、その中間圧用の吸入圧縮部を設けたり、ふたつの低圧吸入圧縮部とこのふたつの低圧吸入圧縮部からの中間圧の冷媒ガスを合わせて高圧圧縮吸入圧縮部へ送るようとする。

【0018】この発明の気体圧縮機は、上述の2段目の圧縮用に戻す冷媒ガスを冷却器400を通して熱交換する冷冻サイクルにも適用できるが、必ずしも冷却器を通す必要はない。

### 【0019】

【発明の実施の形態】この発明の実施の形態を、以下、図1～図7を参照して説明する。

【0020】図1は、この発明の一実施の形態を示す概断面図、図2は、図1のI—I—I—I線断面図、図3は、図1のII—II—II—II線断面図、図4、図5および図6は、それぞれ図1の気体圧縮機のリアサイドブロック、フロントサイドブロックおよびフロントヘッドのA矢示図、図7は、図1の気体圧縮機の2段圧縮行程を示すブロック図である。

【0021】図1において、1はシリンドラブロック、2はリアサイドブロック、3はフロントサイドブロック、4はフロントヘッド、5はケーシングである。

【0022】シリンドラブロック1は、両端面をリアサイドブロック2とフロントサイドブロック3によって塞が

れ、図2に示すように、内部にはば断面稍円形のシリンダ室6が形成されている。上記リアサイドブロック2の外側端面は上記ケーシング5により塞がれ、リアサイドブロック2とケーシング5との間には高圧吐出室7が形成されている。また、フロントサイドブロック3の外側端面は上記フロントヘッド4により塞がれ、フロントサイドブロック3とフロントヘッド4との間には中間圧吐出室8が形成されている。

【0023】9はロータで、このロータ9は、ロータ軸10により上記シリング室6内に回転自在に構架され、シリング室6の内周面の、後に説明する、複数の短径部に所定の間隔をもって近接している。上記ロータ軸10は、リアサイドブロック2の軸受部11とフロントサイドブロック3の軸受部12により支持され、フロント側はフロントヘッド4側に伸びて、フロントヘッド4に装着された電磁クラッチ13と係合し、ベルト14、ブーリ15、電磁クラッチ13を介して自動車のエンジンの回転動力が伝達され、シリング室6内でロータ9を回転するようになっている。

【0024】【シリング室内部】次に、シリング室6内部の詳細を説明する。

【0025】図2に示すように、ロータ9には5個のペーン溝16がロータ中心からやや傾けた放射状に形成されている。これらのペーン溝16には、溝内を進退自在、かつ、シリング室6の内周面に接するペーン17が挿入されている。また、断面はば断面稍円形のシリング室6の内周面の2か所の短径部6a、6bはロータ軸中心の内円弧となつており、ロータ9の外径部がこれらの短径部6a、6bと所定の間隔をもって近接している。

【0026】上記ペーン溝16の底部には、背压室18が設けられ、この背压室18には、後に詳細に説明するように、シリング室6内の角度位置に応じて適当な背圧が付加されるようになっている。

【0027】上記短径部6a、6bの付近、ロータ9の進行方向には、高サイドブロック2、3、及び吸入孔19、20、19-2、20-2が配設されている(図4、図5参照)。また、短径部6a、6bの付近、吸入孔19、20、19-2、20-2の反対側には、シリングブロック1に吐出孔21、22が配設されている。そして、ひとつの短径部6a(または6b)付近の吸入孔19、19-2(または20、20-2)から、その隣の短径部6b(または6a)付近に配設された吐出孔22(または21)にかけてのシリング室6とロータ9との間に、複数の吸入圧縮部23、24が形成され、これらの吸入圧縮部23、24には、シリング室6内で回転するロータ9とひと組のペーン17、17により隔壁生成される圧縮室25がその体積を変化させながら通過するようになっている。

【0028】【冷媒の流路と冷媒の2段圧縮過程】次に、図7を参照しながら、この気体圧縮機内の冷媒の流

路を説明する。

【0029】気体圧縮機には、図1、図3に示した吸入口26、図1に示した吐出口27および外部冷媒ガス供給口28が開口しており、冷凍システムの配管に接続されるようになっている。例えば、図8に示した冷凍システムに使用する場合は、吸入口26をアクチュエレーター700に通じる配管に、吐出口27を放熱器200に通じる配管に、また、外前冷媒ガス供給口28を冷却器400の熱交換通路400aに通じる配管に、それぞれ接続する。

【0030】冷凍システムの低圧側に接続される吸入口26は、吸入連通路29、フロントサイドブロック3の連通孔31を介して上記吸入孔19に連通し、この吸入口孔19は、低圧冷媒ガスを吸入する低圧吸入孔となつておらず、低圧吸入孔19のある吸入圧縮部23は、低圧冷媒ガスを吸入して圧縮する低圧吸入圧縮部となっている。なお、リアサイドブロック2側の低圧吸入孔19-2も、シリングブロック1に貫通したシリングブロック低圧連通路33によりフロントサイドブロック3側の低圧吸入孔19と連通している。冷凍システムの高圧側に接続される吐出口27は、上記高圧吐出室7に連通している。冷凍システムの中間圧側に接続される外部冷媒ガス供給口28は、上記中間圧吐出室8に連通している。

【0031】低圧吸入圧縮部23の吐出孔21は、中間圧に圧縮した冷媒ガスを吐出する中間圧吐出孔となっていて、吐出弁30、連通路47を介して上記中間圧吐出室8に連通している。なお、上記吐出弁30は、シリングブロック1の吐出孔21周辺に形成された弁座、リードバルブ、このリードバルブの過大な曲りを抑えてバッカアップするや肉厚のバルブガイド等からなる従来周知の吐出弁である。

【0032】もう一方の吸入圧縮部24の吸入孔20もまた中間圧吐出室8に連通しており、この吸入孔20は、中間圧冷媒ガスを吸入する中間圧吸入孔、吸入圧縮部24は、中間圧から高圧に冷媒ガスを圧縮する高圧圧縮吸入圧縮部となっている。

【0033】なお、フロントサイドブロック2の上記の吸入孔19と、リアサイドブロック2の上記の吸入孔19-2、中間圧吸入孔20-2は、それぞれ両サイドブロック2、3のシリング室6に面する端面に設けられた凹所となっており、フロントサイドブロック2の上記の吸入孔20は貫通して中間圧吐出室8と連通している。

【0034】リアサイドブロック2側の中間圧吸入孔20は、シリングブロック1に貫通したシリングブロック中間圧連通路32によりフロントサイドブロック3側の中間圧吸入孔20と連通している。

【0035】高圧圧縮吸入圧縮部24の高圧吐出孔22は吐出弁34(図2参照)、高圧冷媒通路44、45、46(図4参照)および油分離器35(図1参照)を介して高圧吐出室7と連通している。なお、上記吐出弁3

4は、吐出弁30と同様にシリンドブロック1の吐出孔22周辺に形成された弁座、リードバルブ、このリードバルブの過大な曲りを抑えてバックアップするやや肉厚のバルブガイド等からなる従来周知の吐出弁である。

【0036】気体圧縮機の冷媒吸入・圧縮動作は以下のようになる。

【0037】気体圧縮機のロータ9の回転により、低圧吸入圧縮部23に位置する圧縮室25は、ロータ9の回転に伴って、体積増加過程で低圧吸入孔19、19-2から約3.5MPaのCO<sub>2</sub>冷媒ガスを吸出し、体積減少過程でこれを中間圧に圧縮して中間圧吐出孔21から吐出弁30を介して中間圧吐出室8へ送り込む。この中間圧吐出室8には、外部冷媒供給口28から中間圧の冷媒が送り込まれており、3.5MPaから1.0MPaに圧縮する場合、中間圧がほぼその中間の6.5~7MPaになるように冷凍システムの減圧装置で制御されている。

【0038】この間、高圧圧縮吸込圧縮部24に位置する圧縮室25では、体積増加過程で中間圧吸入孔20、20-2から中間圧吐出室8の約6.5MPaの冷媒ガスを吸出し、体積減少過程でこれを約1.0MPaの高圧に圧縮して高圧吐出孔22から吐出弁34、油分離器35を介して高圧吐出室7へ送り込む。高圧吐出室7の約1.0MPaの高圧冷媒は、吐出口27から外部へ送り出される。

【0039】このように、低圧吸入圧縮部23の第1段目の圧縮と、高圧圧縮吸込圧縮部24の第2段目の圧縮の2段の圧縮により、例えば、3.5MPaから1.0MPaというような、高い圧力差の圧縮を実現できる。外部冷媒ガス供給口28から流入する冷媒ガスの流量により中間圧は自動的に調整され、第1段目と第2段目の圧縮室の体積を同一にすることができる。

【0040】【背圧と潤滑】上述の気体圧縮機では、ペーン17はシリンドラ室内面盾面に押圧される。この押圧力はペーン自体の回転による遠心力に加えて、背圧室18に加わる背圧によっている。この背圧は、低圧吸入圧縮部23では高圧圧縮吸込圧縮部24よりもやや低圧とすることが望ましい。なぜならば、低圧吸入圧縮部23では圧縮する圧力が6.5MPa程度で、この程度の圧力に打ち勝ってペーン17をシリンドラ室内面盾面に押すのにあまり高い背圧を加えると、ペーンとシリンドラ室とのシールは良好になるが、動力損失が大きくなり過ぎるので対し、高圧圧縮吸込圧縮部24では圧縮する圧力が1.0MPa程度と高く、この高圧に打ち勝ってペーン17をシリンドラ室内面盾面に押すには、高めの背圧が必要だからである。

【0041】そこで、この発明では、中間圧吐出室8の底部に中間圧油貯留室36、高圧吐出室7の底部に高圧油貯留室37を設け、中間圧油貯留室36の潤滑油が低圧吸入圧縮部23を通過中のペーン17を押圧するため

の背圧室18へ、高压油貯留室37の潤滑油が高压圧縮吸込圧縮部24を通過中のペーン17を押圧するための背圧室18へ供給されるようになっている。

【0042】すなわち、中間圧油貯留室36の潤滑油は、フロント油孔38から軸受部12へ送られて軸受を潤滑し、フロント絞り孔39で更に減圧されて両サイドブロック2、3の中間背圧油供給回路40へ送られ、この中間背圧油供給回路40と接する低圧吸入圧縮部23通過中の背圧室18に供給される。一方、高压油貯留室37の潤滑油は、リア油孔41から軸受部11へ送られ軸受を潤滑し、リア絞り孔42で更に減圧されて両サイドブロック2、3の高背圧油供給回路43へ送られ、この中間背圧油供給回路43と接する高圧圧縮吸込圧縮部24通過中の背圧室18に供給される。なお、リアサイドブロック2の中間背圧油供給回路40への中間背圧油の供給路と、フロントサイドブロック3の高背圧油供給回路43への高背圧油の供給路は図示を省略する。

【0043】中間背圧油供給回路40の圧力は、高背圧油供給回路43の圧力よりも低く、低圧吸入圧縮部23を通過中のペーンも、高圧圧縮吸込圧縮部24を通過中のペーンも、それぞれに適合した背圧が加えられ、過大な動力損失なしで、良好なペーンとシリンドラ室とのシールが確保される。

【0044】なお、背圧室17から漏れ出す潤滑油は、ロータ9とペーン17との摺動面、ペーン17とシリンドラ室との摺動面の潤滑にも使用される。また、中間圧油貯留室36、高压油貯留室37の潤滑油は、図示省略の経路を経てロータ9、ペーン17と両サイドブロック2、3との接続面へも送られ、その潤滑にも使用される。潤滑油は、上記油分離器35で冷媒から分離され、高压油貯留室37へ戻される。中間圧油貯留室36への潤滑油の回収は、中間圧吐出室8に一旦収容される冷媒から分離回収によっている。

【0045】

【発明の効果】以上詳細に説明したように、この発明の気体圧縮機は、互いに等しい体積の複数の圧縮室が低圧吸入圧縮部と高圧圧縮吸込圧縮部とを順次通過しながら、低圧吸入圧縮部では、低圧の冷媒ガスを低圧吸入孔から吸い込んで中間圧の冷媒ガスに圧縮して中間圧吐出孔へ吐出し、高圧圧縮吸込圧縮部では、上記の中間圧の冷媒ガスおよび外部から供給される補充用の冷媒ガスを中間圧吸入孔から吸い込んで高圧の冷媒ガスに圧縮して高圧吐出孔へ吐出するようにしたから、フロン等従来の冷媒を用いたペーンロータリ型気体圧縮機と同様のロータ、ペーン、シリンドラを使用でき、簡単でローコスト、小型な気体圧縮機とすることができ、二酸化炭素、エチレン、エタン、酸化窒素等を冷媒とした高い圧力差の気体圧縮機を実現できた。

【図面の簡単な説明】

【図1】この発明の一実施の形態を示す縦断面図。

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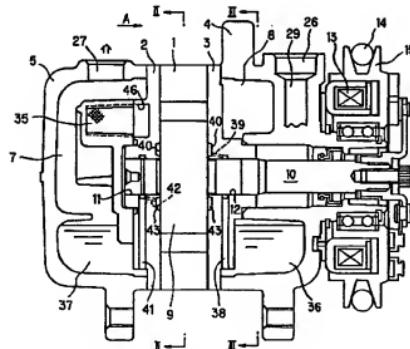
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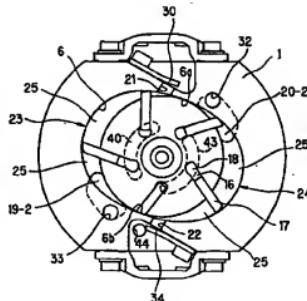
- 【図2】図1のI—I—I—I断面図。  
 【図3】図1のI—I—I—I断面図。  
 【図4】図1のリアサイドブロックのA矢示図。  
 【図5】図1のフロントサイドブロックのA矢示図。  
 【図6】図1のフロントヘッドのA矢示図。  
 【図7】2段圧縮工程に冷媒を戻す方式の蒸気圧縮式冷凍サイクルの説明図。  
 【図8】図1の気体圧縮機の2段圧縮行程を示すブロック図。  
 【図9】図6の蒸気圧縮式冷凍サイクルのモリエル線図。  
 【符号の説明】  
 6 シリンダ室  
 6a 短径部  
 6b 短径部  
 7 高圧吐出室  
 8 中間圧吐出室  
 9 ロータ  
 10 ロータ軸  
 16 ベーン管

- 17 ベーン  
 18 背圧室  
 19 低圧吸入孔  
 19-2 低圧吸入孔  
 20 中間圧吸入孔  
 20-2 中間圧吸入孔  
 21 中間圧吐出孔  
 22 高圧吐出孔  
 23 低圧吸入圧縮部  
 10 24 高圧圧縮吸入圧縮部  
 25 圧縮室  
 26 吸入口  
 27 吐出口  
 28 外部冷媒ガス供給口  
 36 中間圧油貯留室  
 37 高圧油貯留室  
 100 圧縮機  
 200 放熱器  
 400 冷却器  
 20 600 蒸発器

【図1】



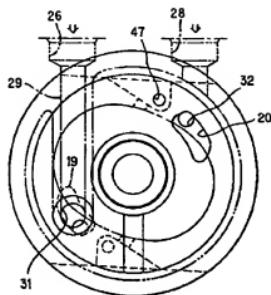
【図2】



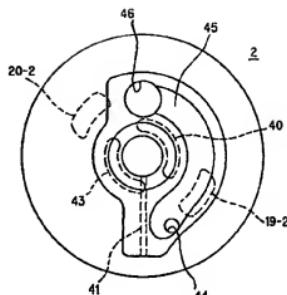
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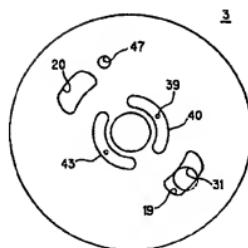
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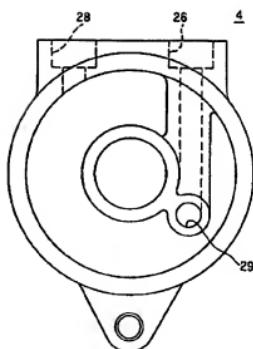
【図4】



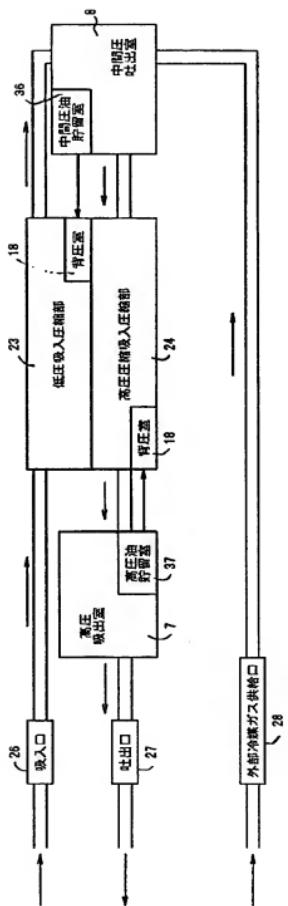
【図5】



【図6】



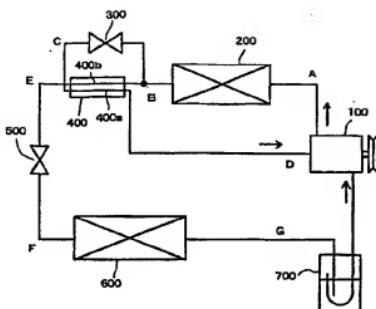
【図7】



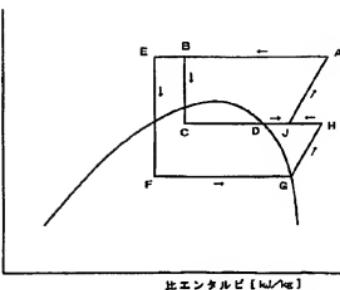
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【図8】



【図9】



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 DD23 DD25 DD40